A commented translation of Hans Richter's early work "The isotropic law of elasticity"

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Abstract

We provide a faithful translation of Hans Richter's important 1948 paper "Das isotrope Elastizitätsgesetz" from its original German version into English. Our introduction summarizes Richter's achievements.

Key words: nonlinear elasticity, isotropic tensor functions, hyperelasticity, logarithmic stretch, volumetricisochoric split, Hooke's law, finite deformations, isotropy

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Introduction

Shortly after the second world war, in a series of papers [23, 24, 25, 26] from 1948 - 1952, Hans Richter (1912 - 1978) laid down his general format of isotropic nonlinear elasticity based on a rather modern approach with direct tensor notation. By translating his work "Das isotrope Elastizitätsgesetz" [23], we aim at making his development, which precedes later work in the field by several decades, accessible to the international audience.

Let us briefly summarize Richter's achievement in this paper. He uses, for the time, rather advanced methods of matrix analysis (including the theory of primary matrix functions [12]) and employs the left polar decomposition [11, 22, 20] of the deformation gradient F = VR into a stretch $V \in \text{Sym}^+(3)$ and a rotation $R \in \text{SO}(3)$. For Richter, the "physical stress tensor" is the Cauchy stress tensor $\sigma \in \text{Sym}(3)$. From the coaxiality between σ and V for an isotropic response, he deduces the representation formula for isotropic tensor functions (the *Richter representation*, see (2.6))

$$\sigma = g_1(I_1, I_2, I_3) \cdot \mathbb{1} + g_2(I_1, I_2, I_3) \cdot V + g_3(I_1, I_2, I_3) \cdot V^2$$

$$(0.1)$$

(predating the Rivlin-Ericksen representation theorem [27] by 7 years) where g_i , i = 1, 2, 3 are scalar valued functions of the invariants I_{ν} , $\nu = 1, 2, 3$, with

$$I_1 = \operatorname{tr}(V), \quad I_2 = \frac{1}{2}\operatorname{tr}(V^2), \quad I_3 = \det V.$$

Alongside, Richter introduces the logarithmic stretch tensor $L = \log V$ without citing the previous work of Hencky [7, 9, 8, 10, 16, 18, 19, 17, 21]. He then turns to the question of what happens if the relation

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(0.1) is derived from a stored energy $W(I_1, I_2, I_3)$, i.e. when (0.1) is consistent with hyperelasticity. He obtains the correct representation (see (3.11) in his text)

$$\sigma = \frac{\partial W}{\partial I_3} \cdot \mathbb{1} + \frac{1}{I_3} \cdot \frac{\partial W}{\partial I_1} \cdot V + \frac{1}{I_3} \cdot \frac{\partial W}{\partial I_2} \cdot V^2, \qquad W = W(I_1, I_2, I_3).$$
(0.2)

In the next section, Richter introduces the *multiplicative split* of the elastic stretch V into volume preserving (isochoric) parts and volume change (see (4.1))

$$V = \frac{V}{(\det V)^{\frac{1}{3}}} \cdot (\det V)^{\frac{1}{3}} \cdot \mathbb{1}$$
(0.3)

and he observes that the logarithmic stretch tensor additively separates both contributions by using the classical deviator operation (see (4.2)) such that

$$\log V = \operatorname{dev} \log V + \frac{1}{3} \operatorname{tr}(\log V) \cdot \mathbb{1} = \log \left(\frac{V}{(\det V)^{\frac{1}{3}}}\right) + \frac{1}{3} \log \det V \cdot \mathbb{1}, \quad \operatorname{dev} X = X - \frac{1}{3} \operatorname{tr}(X) \cdot \mathbb{1}.$$
(0.4)

He also observes that the invariants based on the logarithmic stretch tensor satisfy certain algebraic relations, cf. [3]. In Richter's fifth section, he introduces the *volumetric-isochoric split*

$$W(F) = W_{\text{iso}} \left(\operatorname{dev} \log V \right) + W_{\text{vol}} \left(\operatorname{tr}(\log V) \right)$$
$$= W_{\text{iso}} \left(\log \left(\frac{V}{(\det V)^{\frac{1}{3}}} \right) \right) + W_{\text{vol}} \left(\log \det V \right) = \widetilde{W}_{\text{iso}} \left(\frac{V}{(\det V)^{\frac{1}{3}}} \right) + \widetilde{W}_{\text{vol}} (\det V)$$

of the stored energy (often erroneously attributed to [6]) and he immediately obtains the important result: An isotropic energy is additively split into volumetric and isochoric parts if and only if the mean

Cauchy stress $\frac{1}{3}$ tr σ is only a function of the relative volume change det V. In that case,

$$\frac{1}{3}\operatorname{tr} \sigma = \frac{1}{\det V} \cdot W'_{\operatorname{vol}}(\log \det V) = \widetilde{W}'_{\operatorname{vol}}(\det V).$$
(0.5)

This result has been rediscovered and re-derived multiple times, e.g. in [2, 13, 28, 4, 5, 14]. In addition, Richter shows that this property of the volumetric-isochoric split is invariant under a change of the reference temperature. Finally, he poses the question whether a linear relation between σ and V in the form (the Hooke's law as he perceives it)

$$\sigma = 2\mu \left(V - \mathbb{1} \right) + \lambda \operatorname{tr}(V - \mathbb{1}) \cdot \mathbb{1}, \tag{0.6}$$

where $\mu > 0$ is the shear modulus and λ is the second Lamé parameter, can be consistent with hyperelasticity. A short calculus reveals that (0.6) is hyperelastic if and only if $2\mu = \lambda$, i.e. for Poisson ratio $\nu = \frac{1}{3}$ (which is approximately satisfied for many metals, e.g. aluminium). For all other values of ν , Hooke's law is incompatible with the hyperelastic approach and Richter proposes to use instead (the quadratic Hencky energy [7, 15])

$$W(F) = \mu \, \| \operatorname{dev} \log V \|^2 + \frac{2\mu + 3\lambda}{6} \, \operatorname{tr}^2(\log V)$$

with the induced stress-strain law

$$\sigma \cdot \det F = \tau = 2\mu \log V + \lambda \operatorname{tr}(\log V) \cdot \mathbb{1}, \qquad (0.7)$$

where τ is the Kirchhoff stress tensor.

We will briefly discuss the constitutive relation (0.6). In order to check hyperlasticity of the Cauchy stress-stretch relation in this case, we use the representation, consistent with (0.2),

$$\sigma(V) = \frac{2\,\mu}{J} D_V W(V) \cdot V, \qquad J = \det V, \tag{0.8}$$

and consider the energy $W(F) = 2\mu \det V[\operatorname{tr}(V) - 4]$. Then $\sigma(V) = 2\mu (V - 1) + 2\mu \operatorname{tr}(V - 1) \cdot 1$.

Since $\operatorname{tr}[\sigma(V)] = 8\mu \operatorname{tr}(V - \mathbb{1})$ and $\operatorname{tr}[\sigma(\alpha \mathbb{1})] = 24\mu (\alpha - 1)$, the Cauchy stress tensor given by (0.6) with $2\mu = \lambda$ is injective (but not bijective, since for $\operatorname{tr}(\sigma) = -K^+ < -24\mu$ there does not exist a stretch $V \in \operatorname{Sym}^+(3)$ such that $\operatorname{tr}(\sigma(V)) = -K^+$). Furthermore, note that

$$[\operatorname{tr}(V)]^2 = (\lambda_1 + \lambda_2 + \lambda_3)^2 = \lambda_1^2 + \lambda_2^2 + \lambda_3^2 + 2(\lambda_1\lambda_2 + \lambda_1\lambda_3 + \lambda_2\lambda_3) = \operatorname{tr}(B) + 2\operatorname{tr}(\operatorname{Cof} B),$$
(0.9)

where λ_i are the singular values of the deformation gradient F. Then

$$2\mu \det V [\operatorname{tr}(V) - 4] = 2\mu \sqrt{\det(B)} \{ \sqrt{\operatorname{tr}(B)} + 2\operatorname{tr}(\operatorname{Cof} B) - 4 \} = 2\mu \sqrt{I_3} \{ \sqrt{I_1 + 2I_2} - 4 \}$$
$$= W(I_1, I_2, I_3), \qquad I_1 = \operatorname{tr}(B), \quad I_2 = \operatorname{tr}(\operatorname{Cof} B), \quad I_3 = \det B.$$
(0.10)

For this energy, the weak empirical inequalities [30] $\frac{\partial W}{\partial I_1} > 0$ and $\frac{\partial W}{\partial I_2} > 0$ are satisfied. The principal Cauchy stresses are given by $\sigma_i = 2\mu \cdot (\lambda_i - 1 + (\lambda_1 + \lambda_2 + \lambda_3 - 3))$, which shows that the tension-extension (TE) inequalities and the Baker-Ericksen (BE) inequalities [1], given by

$$0 < \frac{\partial \sigma_i}{\partial \lambda_i} = 2\mu \cdot (1+1) = 4\mu \quad \text{and} \quad 0 < (\sigma_i - \sigma_j)(\lambda_i - \lambda_j) = 2\mu (\lambda_i - \lambda_j)^2$$

respectively, are satisfied as well. We also note that $W(V) = 2\mu \cdot \det V \cdot [\operatorname{tr}(V) - 4]$ is the Shield-transformation [29] of $W^*(F) = 2\mu \cdot [\operatorname{tr}(V^{-1}) - 4]$, where

$$W^{*}(F) = 2\mu \left(\frac{1}{\lambda_{1}} + \frac{1}{\lambda_{2}} + \frac{1}{\lambda_{3}} - 4\right) = g(\lambda_{1}, \lambda_{2}, \lambda_{3})$$
(0.11)

has the Valanis-Landel form [31] and g is convex in $(\lambda_1, \lambda_2, \lambda_3)$; the TE-inequalities are satisfied as well.

Richter's paper is not only written in German, but his notation strongly relies on German fraktur letters, which makes reading his original work rather challenging. In our faithful translation of his paper, we have therefore updated the notation to more current conventions; a complete list of notational changes is provided in Appendix A. Richter's original equation numbering has been maintained throughout.

References

- M. Baker and J. L. Ericksen. "Inequalities restricting the form of the stress-deformation relation for isotropic elastic solids and Reiner-Rivlin fluids". J. Washington Acad. Sci. 44 (1954), pp. 33–35.
- [2] P. Charrier, B. Dacorogna, B. Hanouzet, and P. Laborde. "An existence theorem for slightly compressible materials in nonlinear elasticity". SIAM Journal on Mathematical Analysis 19.1 (1988), pp. 70–85.
- [3] J. C. Criscione, J. D. Humphrey, A.S. Douglas, and W. C. Hunter. "An invariant basis for natural strain which yields orthogonal stress response terms in isotropic hyperelasticity". *Journal of the Mechanics and Physics of Solids* 48.12 (2000), pp. 2445–2465.
- [4] N. Favrie, S. Gavrilyuk, and S. Ndanou. "A thermodynamically compatible splitting procedure in hyperelasticity". *Journal of Computational Physics* 270 (2014), pp. 300–324.
- [5] S. Federico. "Volumetric-distortional decomposition of deformation and elasticity tensor". Mathematics and Mechanics of Solids 15.6 (2010), pp. 672–690.
- P. J. Flory. "Thermodynamic relations for high elastic materials". Transactions of the Faraday Society 57 (1961), pp. 829–838.
- H. Hencky. "Über die Form des Elastizitätsgesetzes bei ideal elastischen Stoffen". Zeitschrift für technische Physik 9 (1928). available at www.uni-due.de/imperia/md/content/mathematik/ag_neff/hencky1928.pdf, pp. 215-220.
- [8] H. Hencky. "Das Superpositionsgesetz eines endlich deformierten relaxationsfähigen elastischen Kontinuums und seine Bedeutung für eine exakte Ableitung der Gleichungen für die zähe Flüssigkeit in der Eulerschen Form". Annalen der Physik 394.6 (1929). available at https://www.uni-due.de/imperia/md/content/mathematik/ag_neff/hencky_ superposition1929.pdf, pp. 617-630.

¹This calculus shows that the Valanis-Landel form is not invariant under the Shield transformation. In addition, the mapping $U \mapsto T_{\text{Biot}} = D_U W(U)$ of the stretch $U = \sqrt{F^T F}$ to the Biot stress tensor T_{Biot} is strictly monotone.

- H. Hencky. "Welche Umstände bedingen die Verfestigung bei der bildsamen Verformung von festen isotropen Körpern?" Zeitschrift für Physik 55 (1929). available at www.uni-due.de/imperia/md/content/mathematik/ag_neff/ hencky1929.pdf, pp. 145-155.
- [10] H. Hencky. "The law of elasticity for isotropic and quasi-isotropic substances by finite deformations". Journal of Rheology 2.2 (1931). available at https://www.uni-due.de/imperia/md/content/mathematik/ag_neff/henckyjrheology31. pdf, pp. 169-176.
- [11] J. Lankeit, P. Neff, and Y. Nakatsukasa. "The minimization of matrix logarithms: On a fundamental property of the unitary polar factor". *Linear Algebra and its Applications* 449 (2014), pp. 28–42. DOI: 10.1016/j.laa.2014.02.012.
- [12] R. J. Martin and P. Neff. "Some remarks on the monotonicity of primary matrix functions on the set of symmetric matrices". Archive of Applied Mechanics 85.12 (2015), pp. 1761–1778. DOI: 10.1007/s00419-015-1017-4.
- J. Murphy and G. Rogerson. "Modelling slight compressibility for hyperelastic anisotropic materials". Journal of Elasticity 131.2 (2018), pp. 171–181.
- [14] S. Ndanou, N. Favrie, and S. Gavrilyuk. "The piston problem in hyperelasticity with the stored energy in separable form". Mathematics and Mechanics of Solids 22.1 (2017), pp. 101–113.
- [15] P. Neff, B. Eidel, and R. J. Martin. "The axiomatic deduction of the quadratic Hencky strain energy by Heinrich Hencky". arXiv:1402.4027 (2014).
- [16] P. Neff, B. Eidel, and R. J. Martin. "Geometry of logarithmic strain measures in solid mechanics". Archive for Rational Mechanics and Analysis 222.2 (2016), pp. 507–572.
- [17] P. Neff and I.-D. Ghiba. "The exponentiated Hencky-logarithmic strain energy. Part III: Coupling with idealized isotropic finite strain plasticity". Continuum Mechanics and Thermodynamics 28.1 (2016), pp. 477–487. DOI: 10. 1007/s00161-015-0449-y.
- [18] P. Neff, I.-D. Ghiba, and J. Lankeit. "The exponentiated Hencky-logarithmic strain energy. Part I: Constitutive issues and rank-one convexity". Journal of Elasticity 121.2 (2015), pp. 143–234. DOI: 10.1007/s10659-015-9524-7.
- [19] P. Neff, J. Lankeit, I.-D. Ghiba, R. J. Martin, and D. J. Steigmann. "The exponentiated Hencky-logarithmic strain energy. Part II: coercivity, planar polyconvexity and existence of minimizers". *Zeitschrift für angewandte Mathematik* und Physik 66.4 (2015), pp. 1671–1693. DOI: 10.1007/s00033-015-0495-0.
- [20] P. Neff, J. Lankeit, and A. Madeo. "On Grioli's minimum property and its relation to Cauchy's polar decomposition". International Journal of Engineering Science 80 (2014), pp. 209–217. DOI: 10.1016/j.ijengsci.2014.02.026.
- [21] P. Neff, I. Münch, and R. J. Martin. "Rediscovering G. F. Becker's early axiomatic deduction of a multiaxial nonlinear stress-strain relation based on logarithmic strain". *Mathematics and Mechanics of Solids* 21.7 (2016), pp. 856–911. DOI: 10.1177/1081286514542296.
- [22] P. Neff, Y. Nakatsukasa, and A. Fischle. "A logarithmic minimization property of the unitary polar factor in the spectral and Frobenius norms". SIAM Journal on Matrix Analysis and Applications 35.3 (2014), pp. 1132–1154. DOI: 10.1137/130909949.
- [23] H. Richter. "Das isotrope Elastizitätsgesetz". Zeitschrift für Angewandte Mathematik und Mechanik 28.7/8 (1948). available at https://www.uni-due.de/imperia/md/content/mathematik/ag_neff/richter_isotrop_log.pdf, pp. 205-209.
- [24] H. Richter. "Verzerrungstensor, Verzerrungsdeviator und Spannungstensor bei endlichen Formänderungen". Zeitschrift für Angewandte Mathematik und Mechanik 29.3 (1949). available at https://www.uni-due.de/imperia/md/content/ mathematik/ag_neff/richter_deviator_log.pdf, pp. 65-75. ISSN: 1521-4001.
- [25] H. Richter. "Zum Logarithmus einer Matrix". Archiv der Mathematik 2.5 (1949). available at https://www.unidue.de/imperia/md/content/mathematik/ag_neff/richter_log.pdf, pp. 360-363. ISSN: 0003-889X. DOI: 10.1007/ BF02036865.
- [26] H. Richter. "Zur Elastizitätstheorie endlicher Verformungen". Mathematische Nachrichten 8.1 (1952), pp. 65–73.
- [27] R. S. Rivlin and J. L. Ericksen. "Stress-deformation relations for isotropic materials". Journal of Rational Mechanics and Analysis 4 (1955), pp. 323–425.
- [28] C. Sansour. "On the physical assumptions underlying the volumetric-isochoric split and the case of anisotropy". European Journal of Mechanics Solids 27.1 (2008), pp. 28–39.
- [29] R. T. Shield. "Inverse deformation results in finite elasticity". Zeitschrift f
 ür angewandte Mathematik und Physik 18.4 (1967), pp. 490–500.
- [30] C. Thiel, J. Voss, R. J. Martin, and P. Neff. "Do we need Truesdell's empirical inequalities? On the coaxiality of stress and stretch". to appear in International Journal of Non-Linear Mechanics (2019). available at arXiv:1812.03053. DOI: 10.1016/j.ijnonlinmec.2019.02.004.
- [31] K.C. Valanis and R.F. Landel. "The strain-energy Function of a hyperelastic material in terms of the extension ratios". Journal of Applied Physics 38.7 (1967), pp. 2997–3002.

The isotropic law of elasticity By *Hans Richter* in Haltingen (Lörrach)

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Abstract

From the demand of the isotropy and of the existence of the thermodynamic potentials a general form of the three-dimensional law of elasticity is stated. In doing so, the logarithmic matrix of relative elongations is used, which permits the separation of the variation of the volume and that of the shape by simply forming the deviator. The resilience energy is exactly the sum of the energy of the variation of the volume and that of the shape, if the average tension depends only on the variation of the volume. For finite deformations, the law of *Hooke* is permissible only in the case $\nu = \frac{1}{3}$.

Aus der Forderung der Isotropie und der Existenz der thermodynamischen Potentiale wird für das räumliche Elastizitätsgesetz eine allgemeine Form angegeben, wobei die logarithmische Dehnungsmatrix verwendet wird, bei der die Trennung in Volum- und Gestaltänderung durch gewöhnliche Deviatorbildung möglich ist. Die elastische Energie ist genau dann die Summe aus Volum- und Gestaltänderungsenergie, wenn die mittlere Spannung nur von der Volumänderung abhängt. Das Hookesche Gesetz ist für endliche Verzerrungen nur bei $\nu = \frac{1}{3}$ zulässig.

En supposant l'isotropie et l'existence des potentiels thermodynamiques, on donne une forme générale de la loi de l'élasticité en se servant d'une matrix logarithmique d'allongement. Ce procédé permet une séparation des changements de volume et de forme par une simple formation de déviateur. Si la tension moyenne ne dépend que du changement de volume, l'énergie d'élasticité est la somme des énergies de changement du volume et de la forme. La loi de *Hooke* n'est admissible que pour $\nu = \frac{1}{3}$.

1 Definitions

In generalization of Hooke's law, a material is called purely elastic if the Cauchy stresses depend in a uniquely reversible way on the stretches. Strictly speaking, however, it is necessary to discuss the heat transfer which occurs in the tensile test; in particular, it is necessary to distinguish between an adiabatic and isothermal law of elasticity. This choice also clarifies what is meant by strains, since strains on the adiabat resp. isotherm can be referred e.g. to the initial state, for which the stresses disappear completely. The strains can also be referred to a stress-free initial state at an arbitrarily chosen initial temperature Θ_0 instead. Then the stress-free state at another temperature Θ corresponds, in the case of an isotropic material, to uniform stretches in all directions, i.e. the thermal expansion. In this manner the law of thermal expansion is included in the elastic law. Of course, the affected material must be assumed not to change permanently by changes in temperature within the considered temperature range.

Thus, we assume a stress-free state at a temperature Θ_0 . Let the deformation of the material into another state be characterized by the matrix F and the related stresses by the stress tensor σ .² We call the material ideally elastic if σ depends uniquely on F and Θ . The material is said to be isotropic if this dependence is invariant under Euclidean rotations.

When solving the problem of finding the most general form of this dependence, one appropriately operates with matrices, where the following abbreviations are used:

 X^T is the matrix obtained by reflecting X over its main diagonal. $(X)_{ik}$ is the entry in the *i*-th row and the *k*-th column of X. det X is the determinant of X. tr X is the sum of the elements on the main diagonal of X: called the trace of X. 1 is the identity tensor. If $f(x) = \sum a_n \cdot x^n$, then, assuming convergence, $f(X) = \sum a_n X^n$.

 $^{^{2}}F$ is the Jacobian matrix: $d\hat{x} = F dx$. σ is the physical stress tensor at the point \hat{x} .

Recall the following simple statements:

$$\operatorname{tr}(X \cdot Y) = \operatorname{tr}(Y \cdot X). \tag{1.1}$$

$$\operatorname{tr}(X \cdot \operatorname{d}\log Y) = \operatorname{tr}(X \cdot Y^{-1} \cdot \operatorname{d}Y) \tag{1.2}$$

if X commutes with Y, but not necessarily with dY.

$$\log(\det X) = \operatorname{tr}(\log X), \qquad (1.3)$$

if $\log X$ is well defined.

For a pure rotation R: $RR^T = \mathbb{1}$. (1.4) For a pure stretch V: $V = V^T$.

Every X can be represented in the form:

$$X = V \cdot R \,, \tag{1.5}$$

where the multiplication is to be read in its functional notation from right to left.

2 Consequence of isotropy

According to (1.5), F can be interpreted as a rotation R followed by a stretch V, where the principal stretch directions of the latter are rotated against those of the coordinate axes. For the case of isotropic materials, the application of R must not have any influence on σ . Therefore, σ is a function of V and Θ . For given F, we can find V by using (1.4) and (1.5) by

$$FF^T = VRR^T V^T = V^2. (2.1)$$

The most general coaxial relation between σ and V which fulfills the invariance under rotations is now, obviously,

$$\sigma = f(V; I_1, I_2, I_3, \Theta), \qquad (2.2)$$

where the I_{ν} are the invariants³ of V.

Instead of V, one can also use a uniquely invertible function of V. As we will see later on, it is appropriate to use the "logarithmic stretch"

$$L = \log V \,, \tag{2.3}$$

which is always defined because of the positive eigenvalues of V. We denote the invariants of L by

$$j = tr(L), \qquad k = tr(L^2) \qquad \text{and} \qquad l = tr(L^3).$$
 (2.4)

Further, from (1.3) and (2.1) we obtain: $j = \frac{1}{2} \operatorname{tr}(\log(FF^T)) = \frac{1}{2} \log(\det(FF^T)) = \log(\det F)$.

Instead of (2.2), we can now write

$$\sigma = f(L; j, k, l, \Theta) \,. \tag{2.5}$$

Here, $tr(\sigma)$, $tr(\sigma L)$ and $tr(\sigma L^2)$ are functions of j, k, l and Θ due to (2.5). If we now define the invariants f_1, f_2 and f_3 as the solutions to the system of equations

$$tr(\sigma) = f_1 tr(1) + f_2 tr(L) + f_3 tr(L^2)$$

$$tr(\sigma L) = f_1 tr(L) + f_2 tr(L^2) + f_3 tr(L^3)$$

$$tr(\sigma L^2) = f_1 tr(L^2) + f_2 tr(L^3) + f_3 tr(L^4)$$

³It is easy to see that here, one of the invariants I_{ν} can be omitted, in contrast to the subsequent formula (2.7).

with, in general, non-vanishing determinant, then we have for

$$X = f_1 \cdot 1 + f_2 \cdot L + f_3 \cdot L^2 : \quad tr(\sigma L^{\nu}) = tr(XL^{\nu}) \quad with \quad \nu = 0, 1, 2.$$

Since σ is coaxial to L, it is completely determined by $tr(\sigma)$, $tr(\sigma L)$ and $tr(\sigma L^2)$. Therefore, $\sigma \equiv X$ holds; i.e.

$$\sigma = f_1(j,k,l,\Theta) \cdot \mathbb{1} + f_2(j,k,l,\Theta) \cdot L + f_3(j,k,l,\Theta) \cdot L^2.$$
(2.6)

Hence, we have found the most general isotropic relation. Using V instead of L, we would correspondingly obtain:

$$\sigma = g_1(I_\nu, \Theta) \cdot \mathbb{1} + g_2(I_\nu, \Theta) \cdot V + g_3(I_\nu, \Theta) \cdot V^2.$$
(2.7)

3 Consequence of the potential

The internal energy of the material per unit volume in the initial state is denoted by

$$E = E(j,k,l,\Theta); \qquad (3.1)$$

the entropy is denoted by

$$S = S(j,k,l,\Theta) \,. \tag{3.2}$$

Then the free energy W takes the form

$$W = E - \Theta \cdot S = W(j, k, l, \Theta).$$
(3.3)

If dA is now the differential of the work done by the element of volume, then

$$dA = -dE + \Theta \cdot dS = -dW - S \cdot d\Theta.$$
(3.4)

Thus for isothermal elastic changes, we have

$$dA = -(dW)_{\Theta = \text{const.}}; \tag{3.5}$$

whereas for adiabatic changes

$$dA = -(dE)_{S=\text{const.}}, \qquad (3.6)$$

where Θ has to be eliminated in (3.1) and (3.2), so that E appears as a function of j, k, l and S.

In order to calculate dA, we transition from a deformation F to the neighboring deformation F + dF. Since a pure rotation has no influence on dA, we can assume that F is a pure stretch. Let e_1 , e_2 and e_3 be the unit vectors in the principal stretch directions of V, which can be interpreted as coordinate vectors. Let σ_1 , σ_2 and σ_3 be the components of σ in these directions. We can use the rectangular parallelepiped spanned by Ve_1 , Ve_2 and Ve_3 as the volume element, which is generated by the stretch V applied to the unit cube. Let us now consider the side which starts from Ve_1 and which is spanned by Ve_2 and Ve_3 . Besides an infinitesimal tilting and change of the surface, this side undergoes a displacement in the e_1 -direction with the magnitude $e_1 \cdot ((V + dF)e_1 - Ve_1) = e_1 dFe_1 = (dF)_{11}$ in the transition from V to V + dF. The work done on the considered side is therefore

$$-\sigma_1 \cdot (\mathrm{d}F)_{11} \cdot (V)_{22} \cdot (V)_{33} = -\det(V) \cdot \frac{(\mathrm{d}F)_{11} \cdot \sigma_1}{(V)_{11}}$$

Thus the entire work done by the volume element is

$$dA = -\det(V) \cdot \sum_{v=1}^{3} \frac{(dF)_{vv} \cdot \sigma_v}{(V)_{vv}} = -\det(V) \cdot \operatorname{tr}(\sigma V^{-1} dF).$$
(3.7)

The deformation V + dF now corresponds to a stretch V + dV, where due to (2.1),

$$(V + \mathrm{d}V)^2 = (V + \mathrm{d}F)(V + \mathrm{d}F^T)$$

or

$$V \cdot \mathrm{d}V + \mathrm{d}V \cdot V = V \cdot \mathrm{d}F^T + \mathrm{d}F \cdot V$$

Multiplying the left side of the equation by σV^{-2} , taking the trace and using (1.1), we find

$$2\operatorname{tr}(\sigma V^{-1}\mathrm{d}V) = \operatorname{tr}(\sigma V^{-1}\mathrm{d}F^T) + \operatorname{tr}(\sigma V^{-1}\mathrm{d}F) = 2\operatorname{tr}(\sigma V^{-1}\mathrm{d}F),$$

since σ is symmetric and coaxial to V. From (3.7) we therefore obtain

$$dA = -\det(V) \cdot \operatorname{tr}(\sigma V^{-1} dV).$$
(3.8)

Hence, due to (1.2), (1.3) and (2.4):

$$\mathrm{d}A = -e^j \cdot \mathrm{tr}(\sigma \,\mathrm{d}L) \,. \tag{3.8*}$$

If we substitute this expression into the isothermal relation (3.5) and use (2.6), then it follows:

$$e^{j} \cdot [f_1 \operatorname{tr}(\mathrm{d}L) + f_2 \operatorname{tr}(L \,\mathrm{d}L) + f_3 \operatorname{tr}(L^2 \,\mathrm{d}L)] = \frac{\partial W}{\partial j} \,\mathrm{d}j + \frac{\partial W}{\partial k} \,\mathrm{d}k + \frac{\partial W}{\partial l} \,\mathrm{d}l \,.$$

Since, by (2.4),

 $\mathrm{d} j = \mathrm{tr}(\mathrm{d} L)\,, \qquad \mathrm{d} k = 2 \, \mathrm{tr}(L \, \mathrm{d} L) \qquad \text{and} \qquad \mathrm{d} l = 3 \, \mathrm{tr}(L^2 \mathrm{d} L)\,,$

we finally conclude that

$$e^{j}f_{1} = \frac{\partial W}{\partial j}, \qquad e^{j}f_{2} = 2\frac{\partial W}{\partial k}, \qquad e^{j}f_{3} = 3\frac{\partial W}{\partial l}$$

and therefore, with (2.6),

$$\sigma e^{j} = \frac{\partial W}{\partial j} \cdot \mathbb{1} + 2 \frac{\partial W}{\partial k} \cdot L + 3 \frac{\partial W}{\partial l} \cdot L^{2}, \qquad W = W(j,k,l,\Theta).$$
(3.9)

Accordingly, from (3.6) we obtain for the adiabatic law:

$$\sigma e^{j} = \frac{\partial E}{\partial j} \cdot \mathbb{1} + 2 \frac{\partial E}{\partial k} \cdot L + 3 \frac{\partial E}{\partial l} \cdot L^{2}, \qquad E = E(j,k,l,S).$$
(3.10)

If we want to omit the introduction of L and use V directly when formulating the law of elasticity, then we appropriately use the following as the invariants of V:

$$I_1 = \operatorname{tr}(V), \qquad I_2 = \frac{1}{2} \operatorname{tr}(V^2), \qquad I_3 = \operatorname{det}(V).$$

Furthermore, according to (2.7), (3.5) and (3.8), an analogous computation leads to the law of elasticity in the form

$$\sigma = \frac{\partial W}{\partial I_3} \cdot \mathbb{1} + \frac{1}{I_3} \cdot \frac{\partial W}{\partial I_1} \cdot V + \frac{1}{I_3} \cdot \frac{\partial W}{\partial I_2} \cdot V^2, \qquad W = W(I_\nu, \Theta)$$
(3.11)

and a corresponding formulation with $E(I_1, I_2, I_3, S)$ instead of W.

4 Transition to the deviators

The introduction of the logarithmic stretch L now proves to be not only appropriate to formulate the law of elasticity as simple as possible, but using L also allows for the decomposition of a deformation into a shape change and volume change by simply taking the deviatoric part, i.e. the same approach as for infinitesimal strains, whereas a corresponding decomposition in terms of V is highly inconvenient. To see this, we decompose the general stretch V into a shape-changing stretch V_g and a volume-changing stretch V_v , i.e. we demand:

$$V = V_g \cdot V_v = V_v \cdot V_g \quad \text{with} \quad \det V_g = 1 \quad \text{and} \quad V_v = \beta \cdot \mathbb{1} \quad \text{with} \quad \beta > 0.$$

$$(4.1)$$

Obviously, (4.1) uniquely determines such a decomposition for each V with det V > 0; namely, for given V,

$$\beta = \sqrt[3]{\det V}$$
 and $V_g = \beta^{-1} \cdot V$

Since V_q commutes with V_v , we can take the logarithm of (4.1):

$$L = L_g + L_v$$
 with $L_g = \log V_g$ and $L_v = \log V_v$. (4.2)

Then, by (1.3), we obtain:

$$\operatorname{tr}(L_g) = \log(\det V_g) = 0, \qquad L_v = \log \beta \cdot \mathbb{1}, \qquad \operatorname{tr}(L_v) = 3\log \beta$$

If, in general, we denote by $\operatorname{dev} D$ the deviator corresponding to the symmetric matrix D, i.e.

$$\operatorname{dev} D = D - \frac{1}{3} \operatorname{tr} D \cdot \mathbb{1} , \qquad (4.3)$$

we can finally write:

$$L_g = \operatorname{dev} L$$
 and $L_v = \frac{1}{3}j \cdot \mathbb{1}$. (4.4)

Thus the change of shape is indeed characterized by the deviator of L. For infinitesimal strains we have $L \approx V - 1$, so that dev L turns into the usual deformation deviator.

If we now introduce the invariants of dev L:

$$y = \operatorname{tr}((\operatorname{dev} L)^2)$$
 and $z = \operatorname{tr}((\operatorname{dev} L)^3)$, (4.5)

then

$$y = k - \frac{1}{3}j^2$$
 and $z = l - jk + \frac{2}{9}j^3$.

We can use j, y and z instead of j, k and l as variables. Then j characterizes the change of volume, whereas y and z characterize the change of shape. As one can easily calculate, (3.9) leads to the formula

$$\frac{1}{3}e^{j}\operatorname{tr}\sigma = \frac{\partial W}{\partial j}$$

$$e^{j}\cdot\operatorname{dev}\sigma = -y\frac{\partial W}{\partial z}\cdot\mathbb{1} + 2\frac{\partial W}{\partial y}\cdot\operatorname{dev}L + 3\frac{\partial W}{\partial z}(\operatorname{dev}L)^{2}$$

$$(4.6)$$

where, in contrast to (3.9), $W = W(j, y, z, \Theta)$ now holds.

A corresponding formula results from (3.10).

Without proof, let us remark that y and z cannot take on all possible values independently of each other, but are restricted by the condition

$$0 \le \frac{z^2}{y^3} \le \frac{1}{6} \,.$$

5 Decomposable elasticity laws

In the elasticity theory of infinitesimal strains the elastic energy can be interpreted as the sum of the energy of the volume and shape change. Since the change of volume is represented by j and the change of shape is represented by y and z, this decomposition is possible for the case of finite strains if and only if

$$W = W_{\text{vol}}(j,\Theta) + W_{\text{iso}}(y,z,\Theta),$$

resp.
$$E = E_{\text{vol}}(j,S) + E_{\text{iso}}(y,z,S)$$

$$(5.1)$$

holds. Then with (4.6):

$$\frac{1}{3}e^j\cdot \mathrm{tr}\, \sigma = \frac{\partial W_{\mathrm{vol}}}{\partial j}(j,\Theta)\,.$$

Thus the average stress depends only on j, i.e. on the change of volume. If, vice versa, tr σ depends only on j, then by (4.6) we obtain

$$\frac{\partial^2 W}{\partial j \partial y} = \frac{\partial^2 W}{\partial j \partial z} = 0\,,$$

which also leads to the form of W in (5.1). Consequently, we can state: The elastic energy can be decomposed into the energy of change of volume and of change of shape if and only if the mean stress depends only on the change of volume.

6 Transition to a new reference temperature

We referred the deformations to the stress-free state at a certain temperature Θ_0 . Now we assume another temperature Θ_1 to be used as initial temperature instead of Θ_0 . For $\sigma = 0$, the temperature Θ_1 corresponds to a certain deformation V_1 with $\log V_1 = L_1$. V_1 is a scalar multiple of the identity tensor; thus dev $L_1 = 0$, $y_1 = z_1 = 0$. Then with (4.6):

$$\frac{\partial W}{\partial j}(j_1, 0, 0, \Theta_1) = 0\,,$$

which leads to the law of thermal expansion:

$$j_1 = \varphi(\Theta_1) \,. \tag{6.1}$$

Since $\hat{F} = FV_1^{-1}$ is the matrix corresponding to the deformation F with respect to the new initial state, we thus have $\hat{V} = VV_1^{-1}$, $\hat{L} = L - L_1$ and hence

$$\widehat{j} = j - j_1, \qquad \widehat{y} = y, \qquad \widehat{z} = z.$$
(6.2)

In formula (4.6), we can now replace j by \hat{j} if we simultaneously substitute W with

$$\widehat{W}\left(\widehat{j}, y, z, \Theta\right) = e^{-j_1} \cdot W\left(\widehat{j} + j_1, y, z, \Theta\right) = e^{-\varphi\left(\Theta_1\right)} \cdot W\left(\widehat{j} + \varphi\left(\Theta_1\right), y, z, \Theta\right).$$
(6.3)

In particular, it follows that the decomposition of the elastic energy, which was discussed in Section 5, is independent of the choice of the reference temperature.

7 Validity of Hooke's law

Due to the formulae found previously, one can impose a wide variety of requirements on the law of elasticity, in particular with respect to the dependence on temperature, and verify if these requirements

can be satisfied. Let us now consider the question whether the common law by Hooke remains valid for finite strains.

Using the Lamé constants, Hooke's law takes the form

$$\sigma = \lambda \cdot \operatorname{tr}(V - 1) \cdot 1 + 2\mu \cdot (V - 1) \tag{7.1}$$

or

$$\sigma = (\lambda \cdot I_1 - 3\lambda - 2\mu) \cdot \mathbb{1} + 2\mu \cdot V.$$
(7.2)

It is obvious that (7.1) is actually derived from the general formula (3.9) for small L.

In order for the isothermal law of elasticity (7.2) to remain valid for finite strains, the following equations must be fulfilled according to (3.11):

$$\lambda I_1 - 3\lambda - 2\mu = \frac{\partial W}{\partial I_3}, \qquad 2\mu I_3 = \frac{\partial W}{\partial I_1} \qquad \text{and} \qquad 0 = \frac{\partial W}{\partial I_2}.$$

This is only possible if $\lambda = 2\mu$, which corresponds to the Poisson ratio $\nu = \frac{1}{3}$. For all other values of ν , Hooke's law cannot be used for finite strains. Instead, one can use the corresponding logarithmic law

$$\sigma e^j = \lambda j \cdot \mathbb{1} + 2\mu L \,, \tag{7.3}$$

which, in the isothermal case, corresponds to the decomposable energy

$$W = \frac{\lambda}{2}j^2 + \mu k = \left(\frac{\lambda}{2} + \frac{\mu}{3}\right) \cdot j^2 + \mu \cdot y.$$

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A List of Symbols

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Our notation	Richter's notation	meaning
X, Y	A, B	arbitrary 3×3 -matrices
X^T	$\overline{\mathfrak{A}}$	transpose of X
$(X)_{ik}$	$(\mathfrak{A})_{ik}$	entry in the <i>i</i> -th row and the k -th column of X
$\det X$	 A	determinant of X
$\operatorname{tr} X$	A.	trace of X
1	E	identity tensor
X^{-1}	\mathfrak{A}^{-1}	inverse of X
F	શ	Jacobian matrix (state of strain)
R	я	pure Euclidean rotation
V	Q	pure stretch
σ	V	stress tensor (state of stress)
Θ	Θ	temperature
I_1, I_2, I_3	I_1, I_2, I_3	invariants of V
$L^{-1, -2, -3}$	<u>2</u>	logarithmic stretch: $L = \log V$
$\frac{-}{i. k. l}$	i. k. l	invariants of L: $i = \operatorname{tr}(L), k = \operatorname{tr}(L^2), l = \operatorname{tr}(L^3)$
f_1, f_2, f_3	f_1, f_2, f_3	coefficient functions
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	J_1, J_2, J_3 J_1, J_2, J_3	coefficient functions
$X = \frac{g_1, g_2, g_3}{X}$	¥	$X = f_1 \cdot 1 + f_2 \cdot L + f_2 \cdot L^2$
21	~	$T = J_1 = J_2 = J_1 = J_3 = J_3$
E	11	internal energy
$\frac{1}{S}$	s	entropy
W	f	free energy
d A	J d A	differential of the work
		unit vectors in the principal stretch directions of V
c_1, c_2, c_3	c_1, c_2, c_3	components of σ in the principal stretch directions of V
01, 02, 03	$0_1, 0_2, 0_3$	components of o in the principal stretch directions of v
	S. S.	stretch in shape, stretch in volume
$\beta^{\prime g, \prime v}$	$\beta^{g, v}$	stretch factor of the stretch in volume V_{i}
	¢. ¢.	$L_v = \log V L_v = \log V$
D_{g}, L_{v}	$\mathfrak{I}_{g}, \mathfrak{I}_{v}$	$L_g = \log r_g, L_v = \log r_v$
dorr D	ĩ	acommon deviator of D
		common deviator of D inversion to of dow L, $u = tr((dow L)^2) = tr((dow L)^3)$
y, z	y, z	Invariants of dev L: $y = tr((dev L)), z = tr((dev L)^{*})$
W, F		volumetric energies
$W_{\rm vol}, E_{\rm vol}$	Γ, U C V	isoshoria operaios
W iso, Diso	G, V	isochoric energies
A resp A	Θ_{0} resp. Θ_{1}	reference temperatures
inder	00 resp. 01	indicator the correspondence to the temperature Θ
		Indicates the correspondence to the temperature Θ_1
$ \frac{\varphi}{\widehat{E}}$	φ	defermention with normeet to the initial state at O
	24	deformation with respect to the initial state at Θ_1
	1	indicates the correspondence to the deformation F'
\wedge, μ	λ, μ	Lame constants
ν	$m = \frac{-}{\nu}$	Poisson modulus