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Construction of polyconvex, anisotropic free-energy functions

The existence of minimizers of some variational principles in finite elasticity is based on the concept of quasiconvexity, introduced by Morrey [6]. This integral inequality is rather complicated to handle. Thus, the sufficient condition for quasiconvexity, the polyconvexity condition in the sense of Ball [1], is a more important concept for practical applications, see also Ciarlet [4] and Dacorogna [5]. In the case of isotropy there exist some models which satisfy this condition. Furthermore, there does not exist a systematic treatment of anisotropic, polyconvex free-energies in the literature. In the present work we discuss some aspects of the formulation of polyconvex, anisotropic free-energy functions in the framework of the invariant formulation of anisotropic constitutive equations and focus on transverse isotropy.

1. Continuum Mechanical and Mathematical Foundations

Let $\mathcal{B} \subset \mathbb{R}^3$ be the body in the reference configuration parametrized in \mathbf{X} . The deformation gradient \mathbf{F} is defined by $\mathbf{F} := \text{Grad}\varphi_t(\mathbf{X})$ with $\det \mathbf{F} > 0$, where φ_t denotes the nonlinear deformation map at time t . The fundamental deformation tensor is the right Cauchy–Green tensor $\mathbf{C} := \mathbf{F}^T \mathbf{F}$. As mentioned before we are interested in polyconvex free-energy functions. Let $W \in C^2(M^{3 \times 3}, \mathbb{R})$ be a scalar-valued energy density, where $M^{3 \times 3}$ denotes the set of real 3×3 matrices, then

Definition: $\mathbf{F} \mapsto W(\mathbf{F})$ is polyconvex if and only if there exists a function $P : M^{3 \times 3} \times M^{3 \times 3} \times \mathbb{R} \mapsto \mathbb{R}$ such that

$$W(\mathbf{F}) = P(\mathbf{F}, \text{Adj}\mathbf{F}, \det \mathbf{F})$$

and $\mathbb{R}^{19} \mapsto \mathbb{R}$, $(X, Y, Z) \mapsto P(X, Y, Z)$ is convex for all points $\mathbf{X} \in \mathbb{R}^3$.

It should be noted that the individual arguments $(\mathbf{F}, \text{Adj}\mathbf{F}, \det \mathbf{F})$ in the above definition can be physically interpreted. \mathbf{F} controls the deformation of an infinitesimal line element, $(\text{Adj}\mathbf{F})^T$ the deformation of an infinitesimal vectorial area element and $\det \mathbf{F}$ the deformation of an infinitesimal volume element. In order to fulfill the principle of objectivity a priori we focus on the so-called reduced constitutive equations for the second Piola–Kirchhoff stresses $\mathbf{S} = 2\partial_{\mathbf{C}}\hat{\psi}(\mathbf{C})$. In the case of transverse isotropy we introduce a material symmetry group $\mathcal{G}_{ti} \subset \text{SO}(3)$ with respect to a local reference configuration, here $\text{SO}(3)$ characterizes the special orthogonal group. Furthermore the concept of material symmetry states that

$$\hat{\psi}(\mathbf{C}) = \hat{\psi}(\mathbf{Q}^T \mathbf{C} \mathbf{Q}) \quad \forall \mathbf{Q} \in \mathcal{G}_{ti}, \mathbf{C}. \tag{1}$$

We say that the function ψ in Equation (1) is a \mathcal{G}_{ti} -invariant function. The material symmetry group is defined by

$$\mathcal{G}_{ti} := \{\mathbf{1}; \mathbf{Q}(\alpha, \mathbf{a}) \mid 0 < \alpha < 2\pi\}, \tag{2}$$

where $\mathbf{Q}(\alpha, \mathbf{a})$ represents all rotations about the preferred direction \mathbf{a} . In order to extend the \mathcal{G}_{ti} -invariant function into a function which is invariant under the special orthogonal group we introduce a so-called structural tensor \mathbf{M} . The invariance group of \mathbf{M} has to preserve the material symmetry group \mathcal{G}_{ti} . For the considered anisotropy class we arrive at $\mathbf{M} := \mathbf{a} \otimes \mathbf{a}$, with $\|\mathbf{a}\| = 1$. This leads to a scalar-valued isotropic tensor function of the form

$$\psi = \hat{\psi}(\mathbf{C}, \mathbf{M}) = \hat{\psi}(\mathbf{Q}^T \mathbf{C} \mathbf{Q}, \mathbf{Q}^T \mathbf{M} \mathbf{Q}) \quad \forall \mathbf{Q} \in \text{SO}(3). \tag{3}$$

Thus it is possible to formulate the free-energy in terms of the so-called principal invariants and the mixed invariants:

$$I_1 = \text{tr} \mathbf{C}, \quad I_2 = \text{tr}[\text{Cof} \mathbf{C}], \quad I_3 = \det \mathbf{C}, \quad I_4 = \text{tr}[\mathbf{C} \mathbf{M}], \quad I_5 = \text{tr}[\mathbf{C}^2 \mathbf{M}], \tag{4}$$

in this context see e.g. [2], [3] and [9]. For the free-energy function we assume the general form $\psi = \hat{\psi}(I_i | i = 1, \dots, 5) + c$, where we have introduced the constant $c \in \mathbb{R}$ in order to fulfill the non-essential normalization condition $\psi(\mathbf{1}, \mathbf{M}) = 0$. Furthermore, the condition $\psi = \hat{\psi}(\mathbf{C}, \mathbf{M}) = \hat{\psi}(\mathbf{Q}^T \mathbf{C} \mathbf{Q}, \mathbf{M})$ holds for all $\mathbf{Q} \in \mathcal{G}_{ti}$, which reflects (1).

2. Polyconvex Anisotropic Free-Energies

In the following we assume an additive decomposition of the free-energy function in isotropic terms ψ_i^{iso} and anisotropic terms ψ_j^{ti} , i.e.

$$\psi = \sum_i \psi_i^{iso}(I_1, I_2, I_3) + \sum_j \psi_j^{ti}(I_1, I_2, I_3, I_4, I_5). \quad (5)$$

For the isotropic ones we can choose some well-known formulations from the literature, see e.g. [4]. Some anisotropic terms are discussed in the following, for details see [7] and [8]. It should be noted that direct extensions of the small strain theory to large strain formulations by replacing the linear strain tensor with the Green-Lagrange strain tensor $\mathbf{E} := \frac{1}{2}(\mathbf{C} - \mathbf{1})$ are a priori not polyconvex. Furthermore, the often used polynomial invariants

$$\mathbf{F} \mapsto \text{tr}(\mathbf{F}^T \mathbf{F} \mathbf{M}) \text{tr}(\mathbf{F}^T \mathbf{F}) = \text{tr}[\mathbf{C} \mathbf{M}] \text{tr} \mathbf{C} = I_1 I_4 \quad \text{and} \quad \mathbf{F} \mapsto \text{tr}[\mathbf{F}^T \mathbf{F} \mathbf{F}^T \mathbf{F} \mathbf{M}] = \text{tr}[\mathbf{C}^2 \mathbf{M}] = I_5 \quad (6)$$

are not polyconvex, see [7], [8]. That means that the functions $c^+ I_5$ and $c^+ I_1 I_4$ can not be used in this form. In order to derive further ansatz functions it seems reasonable to construct a convex polynomial mixed invariant with respect to $\text{Adj} \mathbf{F}$, which reflects the deformation of a preferred area element in some sense. For this we take into account the Cayley-Hamilton theorem and multiply the characteristic polynomial in \mathbf{C} with $\mathbf{C}^{-1} \mathbf{M}$. This leads with $\text{Cof} \mathbf{C} = \text{Adj} \mathbf{C}$ to the expression

$$\text{Cof}[\mathbf{C}] \mathbf{M} = \mathbf{C}^2 \mathbf{M} - I_1 \mathbf{C} \mathbf{M} + I_2 \mathbf{M}. \quad (7)$$

Note that $\text{Cof}[\mathbf{C}]$ is a quadratic function in the \mathbf{C} . The trace of Equation (7) is the polyconvex polynomial invariant

$$K_1 := \text{tr}[\text{Cof}[\mathbf{C}] \mathbf{M}] = I_5 - I_1 I_4 + I_2. \quad (8)$$

The proof of the convexity of the powers of K_1 is straightforward, see [7]. Expressing the invariant K_1 in the form

$$K_1 = \text{tr}[\text{Cof}[\mathbf{C}] \mathbf{M}] = \text{Cof}[\mathbf{F}^T \mathbf{F}] : \mathbf{a} \otimes \mathbf{a} = \|\text{Cof}[\mathbf{F}] \mathbf{a}\|^2, \quad (9)$$

we can give a rather simple geometric interpretation of this polynomial invariant. $\sqrt{K_1} = \|\text{Cof}[\mathbf{F}] \mathbf{a}\|$ controls the deformation of an area element with unit normal \mathbf{a} . With the same arguments we can construct the function

$$K_2 := \text{tr}[\text{Cof}[\mathbf{C}](\mathbf{1} - \mathbf{M})] = I_1 I_4 - I_5, \quad (10)$$

which is polyconvex. The proof is omitted here. K_2 is associated to the deformation of an area element with a normal lying in the isotropy plane. For the polyconvex functions (8) and (10) we can give a simple geometric interpretation; further, more abstract polyconvex functions are e.g.

$$\psi_1^{ti} = \alpha_1 K_1 / I_3^{1/3}; \quad \psi_2^{ti} = \alpha_2 K_1^2 / I_3^{1/3}; \quad \psi_3^{ti} = \alpha_3 K_2 / I_3^{1/3}; \quad \psi_4^{ti} = \alpha_4 K_2^2 / I_3^{1/3}, \quad (11)$$

with $\alpha_i \in \mathbb{R}^+$ for $i = 1, 2, 3, 4$. A spectrum of anisotropic polyconvex ansatz functions is presented in [7].

3. References

- 1 BALL, J.M.: "Convexity Conditions and Existence Theorems in Non-Linear Elasticity", *Archive of Rational Mechanics and Analysis*, 63, 337-403, 1977.
- 2 BETTEN, J.: "Formulation of Anisotropic Constitutive Equations", in J.P. Boehler (ed.): "Applications of Tensor Functions in Solid Mechanics", CISM Course No. 292, Springer-Verlag, 1987.
- 3 BOEHLER, J.P.: "Introduction to the Invariant Formulation of Anisotropic Constitutive Equations", in J.P. Boehler (ed.): "Applications of Tensor Functions in Solid Mechanics", CISM Course No. 292, Springer-Verlag, 1987.
- 4 CIARLET, P.G.: "Mathematical Elasticity, Vol. 1: Three Dimensional Elasticity", Elsevier Science, North-Holland, 1988.
- 5 DACOROGNA, B.: "Direct Methods in the Calculus of Variations", *Applied Mathematical Science* 78, Springer-Verlag, 1989.
- 6 MORREY, C.B.: "Quasi-Convexity and the Lower Semicontinuity of Multiple Integrals", *Pacific J. Math.*, 2, 25-53, 1952.
- 7 SCHRÖDER, J. & NEFF, P.: "Invariant Formulation of Hyperelastic Transverse Isotropy Based on Polyconvex Free-Energy Functions", accepted for publication in *International Journal of Solids and Structures*, 2001.
- 8 SCHRÖDER, J. & NEFF, P.: "On the Construction of Polyconvex Anisotropic Free-Energy Functions", in Proceedings of the IUTAM Symposium on *Computational Mechanics of Solid Materials at Large Strains*, Ed. C. Miehe, 2001, in press.
- 9 SPENCER, A.J.M., "Theory of Invariants", in: *Continuum Physics Vol. 1*, Academic Press, New York, 239-353, 1971.

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