Some thoughts on the shear problem

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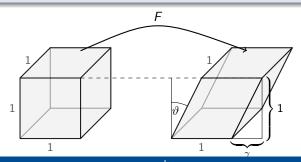


Simple shear deformation [Thiel, Voss, Martin, and Neff 2018b]

A simple shear deformation is a mapping $\varphi \colon \Omega \subset \mathbb{R}^3 \to \mathbb{R}^3$ of the form

$$abla arphi = F_{\gamma} = egin{pmatrix} 1 & \gamma & 0 \ 0 & 1 & 0 \ 0 & 0 & 1 \end{pmatrix} = \mathbb{1} + \gamma \, e_2 \otimes e_1$$

with the amount of shear $\gamma \in \mathbb{R}$.



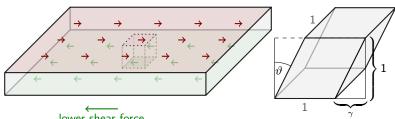
Pure shear stress

A pure shear stress is a stress tensor $T \in Sym(3)$ of the form

$$\mathcal{T}^s = egin{pmatrix} 0 & s & 0 \ s & 0 & 0 \ 0 & 0 & 0 \end{pmatrix} = s(e_1 \otimes e_2 + e_2 \otimes e_1)$$

with the amount of shear stress $s \in \mathbb{R}$.

upper shear force



In isotropic nonlinear elasticity the Cauchy stress tensor is

$$\sigma = \beta_0 \mathbb{1} + \beta_1 B + \beta_{-1} B^{-1}$$

with $\beta_i = \beta_i(I_1(B), I_2(B), I_3(B))$ and $B = FF^T$.

Set
$$\sigma = T^s = \begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$
, $F_{\gamma} = \begin{pmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$

$$\begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} = \sigma = (\beta_0 + \beta_1 + \beta_{-1})\mathbb{1} + \begin{pmatrix} \beta_1 \gamma^2 & (\beta_1 - \beta_{-1})\gamma & 0 \\ (\beta_1 - \beta_{-1})\gamma & \beta_{-1}\gamma^2 & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

$$\Rightarrow \gamma^2 (\beta_1 - \beta_{-1}) = 0 \quad \text{then} \quad \gamma = 0 \quad \text{or} \quad s = 0.$$

Pure shear Cauchy stress never corresponds to a simple shear deformation!

Questions:

- Independent of the elasticity law, which kind of deformations do correspond to pure shear Cauchy stress?
 [Destrade, Murphy, and Saccomandi 2012; Moon and Truesdell 1974; Mihai and Goriely 2011]
- Which of these deformations are suitable to be called 'shear'?
- Which constitutive requirements ensure that only 'shear' deformations correspond to pure shear Cauchy stress?

Which kind of deformations correspond to pure shear stress?

 $B = FF^T$ and $\widehat{\sigma}(B)$ commute for **any** isotropic stress response. $\iff B$ and $\widehat{\sigma}(B)$ are simultaneously diagonalizable.

 $\widehat{\sigma}(B) = T^s$ can be diagonalized to $Q \operatorname{diag}(s, -s, 0) Q^T$ with

$$Q := rac{1}{\sqrt{2}} egin{pmatrix} 1 & -1 & 0 \ 1 & 1 & 0 \ 0 & 0 & \sqrt{2} \end{pmatrix} \in \mathsf{SO}(3) \,.$$

Thus $B = Q \operatorname{diag}(\lambda_1^2, \lambda_2^2, \lambda_3^2) Q^T$ with [Thiel, Voss, Martin, and Neff 2018a]

$$B = \frac{1}{2} \begin{pmatrix} \lambda_1^2 + \lambda_2^2 & \lambda_1^2 - \lambda_2^2 & 0 \\ \lambda_1^2 - \lambda_2^2 & \lambda_1^2 + \lambda_2^2 & 0 \\ 0 & 0 & 2\lambda_3^2 \end{pmatrix} \neq \ F_{\gamma} F_{\gamma}^{T} = \begin{pmatrix} 1 + \gamma^2 & \gamma & 0 \\ \gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}.$$

Which kind of deformations correspond to pure shear stress?

$$\widehat{\sigma}(B) = T^s = \begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \quad \iff \quad B = \frac{1}{2} \begin{pmatrix} \lambda_1^2 + \lambda_2^2 & \lambda_1^2 - \lambda_2^2 & 0 \\ \lambda_1^2 - \lambda_2^2 & \lambda_1^2 + \lambda_2^2 & 0 \\ 0 & 0 & 2\lambda_3^2 \end{pmatrix}.$$

Then F is uniquely determined by triaxial stretch and simple shear

$$F = F_{\gamma} \operatorname{diag}(a, b, c) Q = \begin{pmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} a & 0 & 0 \\ 0 & b & 0 \\ 0 & 0 & c \end{pmatrix} Q$$

up to an arbitrary $Q \in SO(3)$ with

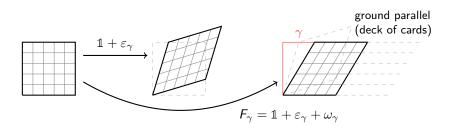
$$a=\lambda_1\lambda_2\sqrt{rac{2}{\lambda_1^2+\lambda_2^2}}\,, \qquad b=\sqrt{rac{\lambda_1^2+\lambda_2^2}{2}}\,, \qquad c=\lambda_3\,, \qquad \gamma=rac{\lambda_1^2-\lambda_2^2}{\lambda_1^2+\lambda_2^2}\,.$$

Linear Elasticity

The linear elastic Cauchy stress $\sigma_{\rm lin}=2\mu\,{\rm dev}\,\varepsilon+\kappa\,{\rm tr}\,\varepsilon$ with $\varepsilon={\rm sym}(F-\mathbb{1})$ and ${\rm dev}\,\varepsilon=\varepsilon-\frac{1}{3}\,{\rm tr}\,\varepsilon\mathbb{1}$ is a pure shear if and only if

$$F = \mathbb{1} + \underbrace{\begin{pmatrix} 0 & \frac{\gamma}{2} & 0 \\ \frac{\gamma}{2} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\varepsilon \in \mathsf{Sym}(3)} + A, \qquad A \in \mathfrak{so}(3).$$

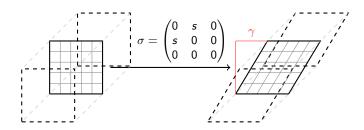
$$F_{\gamma} = \begin{pmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} = \mathbb{1} + \underbrace{\begin{pmatrix} 0 & \frac{\gamma}{2} & 0 \\ \frac{\gamma}{2} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\substack{\varepsilon_{\gamma} \in \operatorname{Sym}(3) \\ \text{infinitesimal pure shear strain}}} + \underbrace{\begin{pmatrix} 0 & \frac{\gamma}{2} & 0 \\ -\frac{\gamma}{2} & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}}_{\substack{\omega_{\gamma} \in \mathfrak{so}(3) \\ \text{infinitesimal rotation}}}.$$



- The deformation F_{γ} is infinitesimally volume preserving, tr $\varepsilon_{\gamma} = 0$.
- The deformation F_{γ} is planar, eigenvalue 1 to eigenvector e_3 .
- The deformation F_{γ} is ground parallel, eigenvectors e_1 and e_3 .

Generalizing from linear elasticity to nonlinear elasticity

- Pure shear Cauchy stress acts only in a plane
- Leonardo da Vinci: "Nessuno effetto è in natura sanza ragione" (No effect is in nature without cause) Codex Atlanticus
- → Nonlinear shear deformation should be planar



Definition: Finite shear deformation [Thiel, Voss, Martin, and Neff 2018b]

- The deformation F is volume preserving, det F = 1.
- The deformation F is planar, eigenvalue 1 to eigenvector e_3 .
- The deformation F is ground parallel, eigenvectors e_1 and e_3 .

 $\implies \text{ there exists } \lambda \in \mathbb{R}_+ \text{ with } \lambda_1 = \lambda \text{, } \lambda_2 = \tfrac{1}{\lambda} \text{ and } \lambda_3 = 1.$

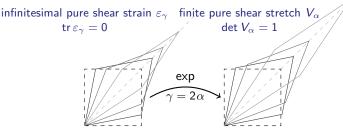
$$\widehat{\sigma}(B) = T^{s} = \begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \implies V = \sqrt{B} = \frac{1}{2} \begin{pmatrix} \lambda_{1} + \lambda_{2} & \lambda_{1} - \lambda_{2} & 0 \\ \lambda_{1} - \lambda_{2} & \lambda_{1} + \lambda_{2} & 0 \\ 0 & 0 & 2\lambda_{3} \end{pmatrix}$$

Finite pure shear stretch

$$V = \frac{1}{2} \begin{pmatrix} \lambda + \frac{1}{\lambda} & \lambda - \frac{1}{\lambda} & 0 \\ \lambda - \frac{1}{\lambda} & \lambda + \frac{1}{\lambda} & 0 \\ 0 & 0 & 2 \end{pmatrix} = \frac{1}{2} \begin{pmatrix} e^{\alpha} + e^{-\alpha} & e^{\alpha} - e^{-\alpha} & 0 \\ e^{\alpha} - e^{-\alpha} & e^{\alpha} + e^{-\alpha} & 0 \\ 0 & 0 & 2 \end{pmatrix}$$

$$= \begin{pmatrix} \cosh(\alpha) & \sinh(\alpha) & 0 \\ \sinh(\alpha) & \cosh(\alpha) & 0 \\ 0 & 0 & 1 \end{pmatrix} = \exp \begin{pmatrix} 0 & \alpha & 0 \\ \alpha & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} =: V_{\alpha}, \quad \alpha := \log \lambda.$$

$$\underset{\text{matrix exponential}}{\text{matrix exponential}} \underset{\text{infinitesimal pure shear strain}}{\text{matrix exponential}}$$



$$\widehat{\sigma}(B) = T^{s} = \begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} \implies F = \begin{pmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} a & 0 & 0 \\ 0 & b & 0 \\ 0 & 0 & c \end{pmatrix} Q.$$

with $\lambda_1 = \lambda$, $\lambda_2 = \frac{1}{\lambda}$, $\lambda_3 = 1$ and $\alpha = \log \lambda$:

Finite simple shear deformation

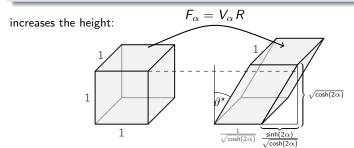
$$\begin{split} F &= \begin{pmatrix} 1 & \tanh(2\alpha) & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} \frac{1}{\sqrt{\cosh(2\alpha)}} & 0 & 0 \\ 0 & \sqrt{\cosh(2\alpha)} & 0 \\ 0 & 0 & 1 \end{pmatrix} Q \\ &= \frac{1}{\sqrt{\cosh(2\alpha)}} \begin{pmatrix} 1 & \sinh(2\alpha) & 0 \\ 0 & \cosh(2\alpha) & 0 \\ 0 & 0 & \sqrt{\cosh(2\alpha)} \end{pmatrix} Q =: F_{\alpha} \,. \end{split}$$

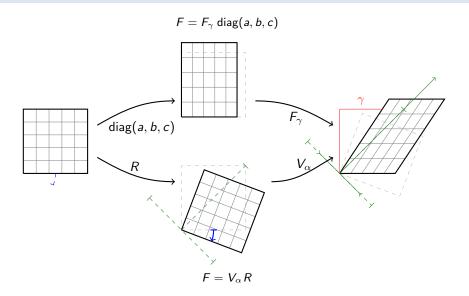
Finite simple shear deformation

A finite simple shear deformation is a mapping $\varphi \colon \Omega \subset \mathbb{R}^3 \to \mathbb{R}^3$ of the form

$$\nabla \varphi = F_{\alpha} = \frac{1}{\sqrt{\cosh(2\alpha)}} \begin{pmatrix} 1 & \sinh(2\alpha) & 0 \\ 0 & \cosh(2\alpha) & 0 \\ 0 & 0 & \sqrt{\cosh(2\alpha)} \end{pmatrix}$$

with the linearization $F_{\alpha} \stackrel{\alpha \ll 1}{\longrightarrow} F_{\gamma}$ and $\gamma = 2\alpha$.





Constitutive requirements in hyperelasticity

Which constitutive requirements ensure that only finite shear deformations correspond to pure shear Cauchy stress?

$$V_{\alpha} = \begin{pmatrix} \cosh(\alpha) & \sinh(\alpha) & 0 \\ \sinh(\alpha) & \cosh(\alpha) & 0 \\ 0 & 0 & 1 \end{pmatrix} = Q \cdot \underbrace{\begin{pmatrix} \lambda & 0 & 0 \\ 0 & \frac{1}{\lambda} & 0 \\ 0 & 0 & 1 \end{pmatrix}}_{\text{pure shear deformation}} \cdot Q^{T} \quad \text{with } \lambda = e^{\alpha},$$

$$\widehat{\sigma}(B) = \begin{pmatrix} 0 & s & 0 \\ s & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix} = Q \begin{pmatrix} s & 0 & 0 \\ 0 & -s & 0 \\ 0 & 0 & 0 \end{pmatrix} \ Q^T, \quad Q = \frac{1}{\sqrt{2}} \begin{pmatrix} 1 & -1 & 0 \\ 1 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}.$$

$$\underbrace{\lambda_1 = \lambda \,, \quad \lambda_2 = \frac{1}{\lambda} \,, \quad \lambda_3 = 1}_{\text{singular values of } F} \qquad \Longrightarrow \qquad \underbrace{\sigma_1 = s \,, \quad \sigma_2 = -s \,, \quad \sigma_3 = 0}_{\text{principal Cauchy stresses}} \,.$$

Constitutive requirements in hyperelasticity

$$I_1 = \operatorname{tr} B = \lambda_1^2 + \lambda_2^2 + \lambda_3^2$$
, $I_2 = \operatorname{tr}(\operatorname{Cof} B) = \lambda_1^2 \lambda_2^2 + \lambda_1^2 \lambda_3^2 + \lambda_2^2 \lambda_3^2$, $I_3 = \det B = \lambda_1^2 \lambda_2^2 \lambda_3^2$

$$\begin{split} \sigma &= \beta_0 \mathbb{1} + \beta_1 B + \beta_{-1} B^{-1} \quad \text{with } \beta_i = \beta_i \big(\mathit{I}_1(B), \mathit{I}_2(B), \mathit{I}_3(B) \big) \\ \beta_1 + \beta_{-1} &= 0 \quad \text{and} \quad \beta_0 = 0 \qquad \forall \; \lambda \in \mathbb{R}_+ \; \text{with } \lambda_1 = \lambda \,, \; \lambda_2 = \frac{1}{\lambda} \,, \; \lambda_3 = 1 \,. \end{split}$$

$$\begin{split} \beta_0 &= \frac{2}{\sqrt{I_3}} \left(I_2 \frac{\partial W}{\partial I_2} + I_3 \frac{\partial W}{\partial I_3} \right), \qquad \beta_1 = \frac{2}{\sqrt{I_3}} \frac{\partial W}{\partial I_1} \,, \qquad \beta_{-1} = -2 \sqrt{I_3} \frac{\partial W}{\partial I_2} \,, \\ &\Longrightarrow \frac{\partial W}{\partial I_1} = \frac{\partial W}{\partial I_2} \quad \text{and} \quad I_2 \frac{\partial W}{\partial I_2} + \frac{\partial W}{\partial I_3} = 0 \qquad \forall \ I_1 = I_2 \geq 3 \,, \ I_3 = 1 \,. \end{split}$$

$$\begin{split} &\sigma_i = \frac{\lambda_i}{\lambda_1 \, \lambda_2 \, \lambda_3} \, \frac{\partial W}{\partial \lambda_i} (\lambda_1, \lambda_2, \lambda_2) & \Longrightarrow \\ &\lambda \, \frac{\partial W}{\partial \lambda_1} + \frac{1}{\lambda} \, \frac{\partial W}{\partial \lambda_2} = 0 \quad \text{ and } \quad \frac{\partial W}{\partial \lambda_3} = 0 \qquad \forall \, \lambda_1 = \lambda \, , \, \, \lambda_2 = \frac{1}{\lambda} \, , \, \, \lambda_3 = 1 \, . \end{split}$$

Constitutive requirements in hyperelasticity

Tension-compression symmetry [Voss, Baaser, Martin, and Neff 2018]

Elastic energy $W \colon \operatorname{GL}^+(3) \to \mathbb{R}$ of the form

$$W(F) = W_{tc}(F) + f(\det F),$$

where $W_{\rm tc}$ is tension-compression symmetric, i.e. $W_{\rm tc}(F^{-1})=W_{\rm tc}(F)$ and f'(1)=0.

Hencky-type [Neff, Ghiba, and Lankeit 2015; Neff, Lankeit, Ghiba, Martin, and Steigmann 2015

Elastic energy $W \colon \operatorname{GL}^+(3) \to \mathbb{R}$ of the form

$$W(F) = \psi(\|\operatorname{dev} \log V\|^2, |\operatorname{tr} \log V|^2)$$

for arbitrary functions $\psi \colon \mathbb{R}^2_+ \to \mathbb{R}$.

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References II

Thank you for your attention